

**SNR-SXR™**  
Surface Normal Rotation  
Monochromator

## U.S. Patent 5,274,435

- Self-Focusing Concave Grating
  - High Throughput
- Grazing Incidence: Soft X-Ray Use
- Stationary Slits
- Fixed Beam Directions
- Fixed Numerical Aperture
- Broadband Tunability

## Specifications

### Mounting

Hettrick, U.S. Patent 5,274,435;  
Spherical Grating

### Angular Deviation

4.5° (Fixed). Nominal graze angle of  
2.25°

### Grating Stage Format

Gold Surface;  
Active Circular Aperture 100 mm

### Grating Groove Density

750 g/mm

### Wavelength Range

10~100 Angstroms (m=1); approx.  
6~50 Angstroms (m=2), depending  
on source intensity

### Fractional Dispersive Resolution

0.167/mm (at Source and Exit Slit)

### Optical Aberration (image tilt)

$\Delta\lambda/\lambda < 0.010$  at 6 mrad Sagittal  
Aperture, 10~50 Angstroms (m=1)

### Meridional Aperture

## Background

Prior grazing incidence monochromators have performed scanning, or tuning of the wavelength transmitted through the exit slit, by use of motions solely within the dispersion plane normal to the grating grooves. Such scanning has comprised rotation of the grating about an axis parallel to its grooves, sometimes accompanied by translation of the grating or rotation and translation of mirrors and slits within this same dispersion plane. This historical constraint has resulted in several performance limitations, particularly when operated at grazing angles of incidence, including 1) a large fractional variation in the aperture as a function of tuned wavelength, 2) a narrow tuning range for efficient diffraction by a blazed grating, 3) a high required precision of grating and mirror rotation and slit translation, and typically 4) defocusing due to the dependence of the grating focal length upon incidence angle.

However, by discarding the geometrical convention of motions exclusively within the grating dispersion plane, and extending scanning to the third dimension, these performance limitations are overcome at grazing incidence.

## Optical Principle

The SNR Monochromator is based on the novel<sup>1</sup> and patented<sup>2</sup> tuning geometry illustrated below. A reflection grating is rotated about an axis normal to its surface. An incident ray now views a groove spacing which has, in effect, increased as projected onto the dispersion plane. Therefore, the wavelength dispersed onto the stationary exit slit is scaled in proportion:

12.5 mrad, on Rowland Circle

**Sagittal Aperture**

0–30 mrad, astigmatic ( $\phi$ )

**Exit Slit Width (Vacuum Selectable)**

- 200  $\mu\text{m}$  at  $0.2^\circ$
- 100  $\mu\text{m}$  at  $0.2^\circ$  (10–13  $\text{\AA}$ )
- 100  $\mu\text{m}$  at  $0.7^\circ$  (13–20  $\text{\AA}$ )
- 100  $\mu\text{m}$  at  $1.2^\circ$  (20–28  $\text{\AA}$ )
- 100  $\mu\text{m}$  at  $1.7^\circ$  (28–37  $\text{\AA}$ )
- 100  $\mu\text{m}$  at  $2.2^\circ$  ( $> 37 \text{\AA}$ )

**Exit Slit Length**

20 mm

**External Drive**

Single Micro-Stepped Motor with Compumotor ZETA6104-57-83 Indexer/Drive w/RS232C Interface Port

**Vacuum Chamber**

Weld-Free 6061 Aluminum, Electroless Nickel Plated; TEFLAT/BLACKFLAT Sealed Knife-edge Ports

**Entrance and Exit Ports**

4.5" Conflat Flange (ICF114)

**User Ports**

Three Ports Accept 2.75" Conflat Flange (ICF63)

**Length**

0.63 meters (Slit-Slit)

**Aperture Center**

Stationary

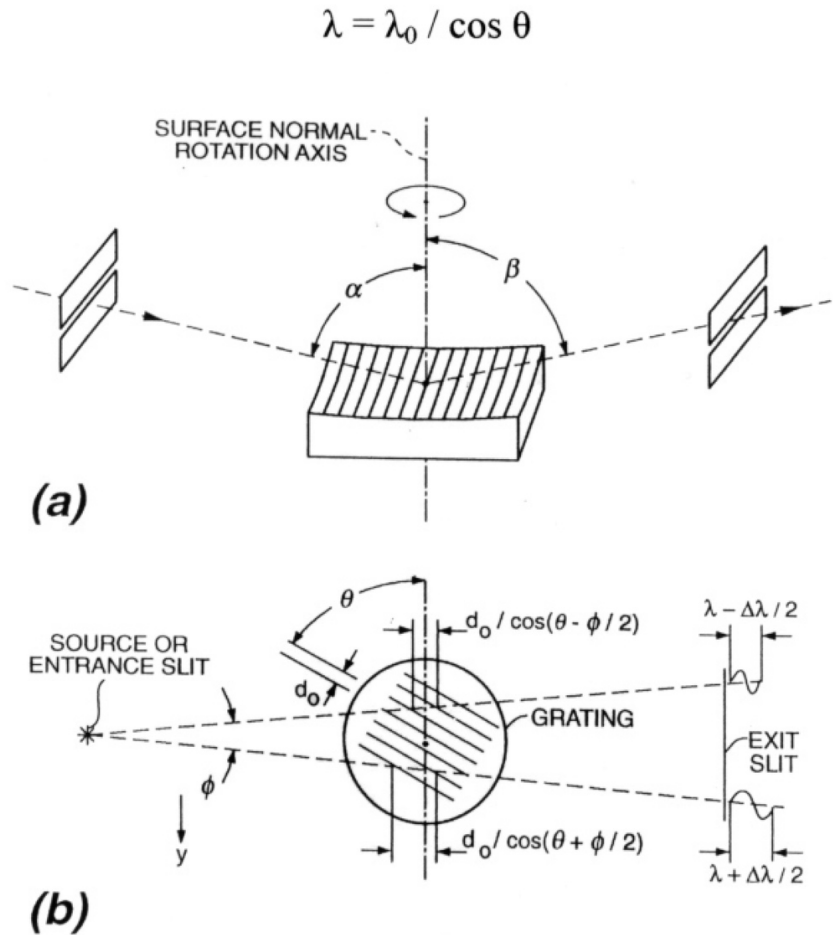


Fig. 1. Geometry of a simple surface normal rotation (SNR) fixed-slit grating monochromator. (a) Three-dimensional perspective where the grating is oriented to diffract the minimum wavelength through the exit slit. (b) Top view of the rotated grooves showing the groove spacings projected upon the sagittal incident rays, resulting in a limit to the spectral resolution. The same rotation technique may be used to construct other optical systems including plane grating designs, those employing auxiliary mirrors, and those where the slit(s) may move.

Because the optical surface is unchanged in position and orientation by such motion, the grating maintains its focusing properties, such as its focal length and numerical aperture at the new wavelength. In the self-focusing geometry where the grating surface is concave, stationary entrance and exit slits can be maintained on the Rowland circle or other desirable focusing condition.

The mechanical advantage provided by the cosine dependence of tuned wavelength upon rotation angle is of great advantage at grazing incidence. In the conventional rotation of a grating within the dispersion plane, the required angular accuracy is a small fraction of the graze angle (for example, 1 part in 1000 of a graze angle of 2 degrees). However, in the present surface normal rotation scheme, the required accuracy is a small fraction of 90 degrees, independent of the graze angle, representing a relaxation of 1 to 2 orders of magnitude.

Furthermore, due largely to the increase in effective groove spacing in proportion to the wavelength, the grating is maintained closer to the blazed condition of specular reflection from the groove facet as wavelength is tuned. This provides a significantly wider tuning range than possible with conventional rotation which tilts the groove facets away from the blazed direction.

The limitation of this simple geometry is the tilt of the image at the exit slit, which increases in linear proportion to the illuminated aperture  $\phi$  in the non-dispersive (sagittal direction). For non-rotating slits, this limits the spectral resolution to:

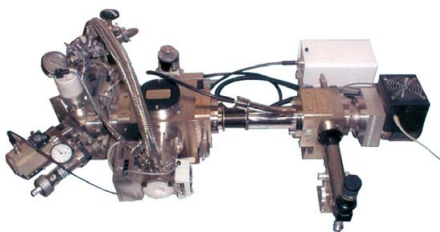
$$\Delta\lambda / \lambda = \phi \tan\theta$$

For example, with  $\phi = 2$  mrad and  $\theta = 78.5$  degrees, a fractional wavelength resolution of less than 1/100 is maintained over a factor five scan in wavelength.

## Construction

Model SNR-SXR-0.6 is a high aperture ( $\Phi = 12.5$  mrad), single-element soft x-ray Monochromator. The grating has a 100 mm circular aperture with grooves extending to the edge. The distance from (slitless) source to exit slit is 628 mm. The fixed angular deviation of 4.5 degrees and gold coated grating provide efficient reflection to wavelengths as short as  $\lambda_{\min} = 10$  Angstroms in first order and to approximately 6 Angstroms in second order. The spectral resolution is determined by the sagittal aperture which may be set by knife-edges at the entrance port of exit slit, over the range of approximately 0 to 30 mrad. A typical setting of 3 mrad (illuminating 2 mm at the exit slit) provides a fractional spectral resolution of 1/160 at 23 Å, 1/68 at 50 Å, and 1/33 at 100 Å. However, the long wavelength performance is improved considerably by employing an exit slit mask containing 6 slits (100  $\mu\text{m}$  wide) at different angles, to match the image tilt over different regions in scanned wavelength. Using the appropriate slit, the resolution is approximately 1/100 over 10–50 Å using a 6 mrad sagittal aperture. An externally mounted micro-stepping motor with Compumotor indexer provides rotational control of the grating scan under vacuum by means of a shaft feedthrough. The slits are also selectable under vacuum using a micrometer shaft feedthrough. Both the grating chamber and the slit chambers are electroless-nickel plated aluminum and are machined square relative to the grating surface and slit mask, enabling alignment by mechanical indication from the chamber exteriors.

The photograph shows a custom system including model SNR-SXR-0.6 and associated optional equipment (not included with base instrument) such as a Manson model 2 soft x-ray source and compact chamber, pumps, gages, mounting table and brackets, CCD, filter assembly, vacuum-selectable aperture and microscope visible alignment system, for calibrating x-ray transmission gratings in the 5-114 Å region.



The SNR geometry is particularly advantageous when a large fixed target must be illuminated by a constant beam size over a broad range in wavelength.

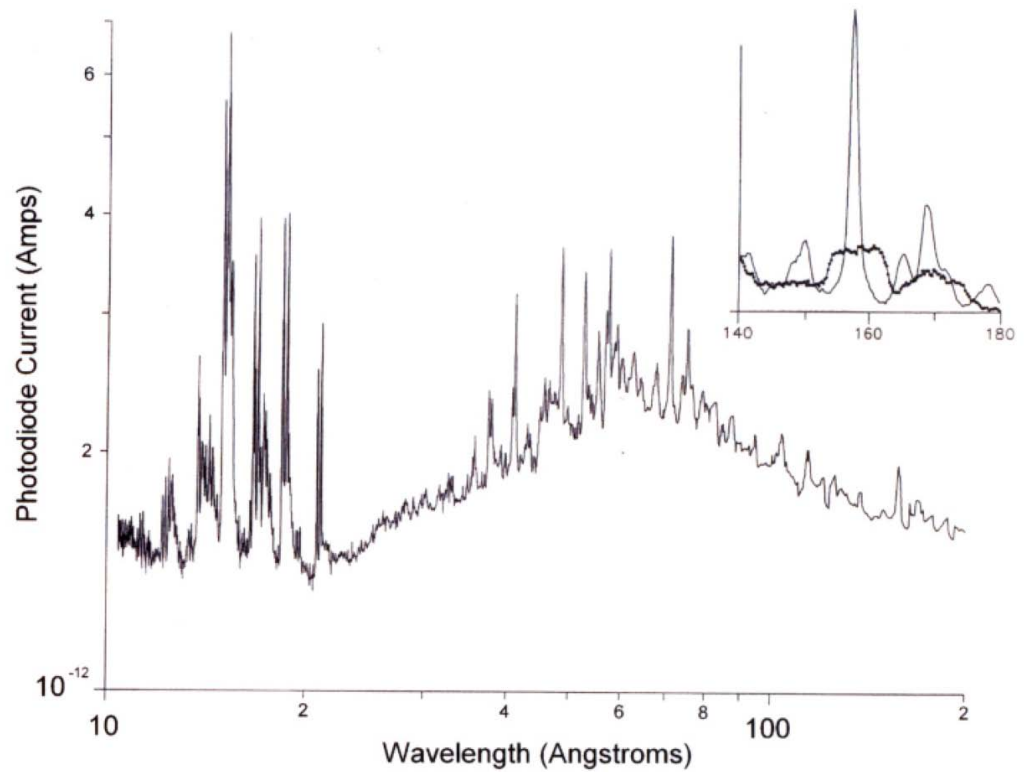


Fig. 2. Spectrum of a type 303 stainless-steel laser-plasma source obtained by using a sagittal aperture of 1 mrad and an exit-slit width of 20  $\mu\text{m}$ . The heavy curve in the inset shows the degradation in spectral resolution caused by an increased (4-mrad) sagittal aperture. The light curve in the inset shows a factor of 6 improvement obtained by tilting the exit slit for optimum performance at a wavelength of 15.8 nm.

<sup>1</sup> M.C. Hettrick, "Surface normal rotation: a new technique for grazing incidence monochromators," *Appl. Opt.* 31, 7174 (1992)

<sup>2</sup> U.S. Patent No. 5,274,435.